

# MICRO-HERMETIC PACKAGING OF OPTICAL DEVICES

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## RELATED APPLICATIONS

**[0001]** This application claims benefit of the following U. S. provisional patent applications:

**[0002]** App. No. 60/393,974 entitled "Micro-hermetic packaging of optical devices" filed 07/05/2002 in the names of Albert M. Benzoni, Henry A. Blauvelt, David W. Vernooy, and Joel S. Paslaski, said provisional application being hereby incorporated by reference as if fully set forth herein;

**[0003]** App. No. 60/466,799 entitled "Low-profile-core and thin-core optical waveguides and methods of fabrication and use thereof" filed 04/29/2003 in the names of David W. Vernooy, Joel S. Paslaski, and Guido Hunziker, said provisional application being hereby incorporated by reference as if fully set forth herein; and

**[0004]** App. No. 60/473,699 entitled "Surface-mounted photodiode for an optical waveguide" filed 05/27/2003 in the names of Henry A. Blauvelt, David W. Vernooy, and Joel S. Paslaski, said provisional application being hereby incorporated by reference as if fully set forth herein.

## BACKGROUND

**[0005]** The field of the present invention relates to optical telecommunication devices. In particular, apparatus and methods are described herein for micro-hermetic packaging of optical devices.

**[0006]** This application is related to subject matter disclosed in:

**[0007]** U.S. non-provisional App. No. 10/187,030 entitled "Optical junction apparatus and methods employing optical power transverse-transfer" filed 06/28/2002 in the names of Henry A. Blauvelt, Kerry J. Vahala, David W. Vernooy, and Joel S. Paslaski, said application being hereby incorporated by reference as if fully set forth herein;

1 **[0008]** U.S. provisional App. No. 60/360,261 entitled "Alignment-insensitive optical  
2 junction apparatus and methods employing adiabatic optical power transfer" filed  
3 02/27/2002 in the names of Henry A. Blauvelt, Kerry J. Vahala, David W. Vernooy, and  
4 Joel S. Paslaski; and

5 **[0009]** U.S. provisional App. No. 60/334,705 entitled "Integrated end-coupled  
6 transverse-optical-coupling apparatus and methods" filed 10/30/2001 in the names of  
7 Henry A. Blauvelt, Kerry J. Vahala, Peter C. Sercel, Oskar J. Painter, and Guido  
8 Hunziker.

9 **[0010]** Many types of optical devices are deployed in many different use environments  
10 for implementing an optical telecommunications system. The proper functioning and  
11 performance of these active and passive devices generally depend on isolating the  
12 devices from an uncontrolled use environment that might otherwise degrade the device  
13 and/or its performance and functioning. Devices are therefore hermetically packaged to  
14 reduce or eliminate the influence of an uncontrolled use environment on the device.  
15 Examples of active optical devices may include but are not limited to semiconductor  
16 lasers, electro-absorption modulators, electro-absorption modulated lasers, electro-optic  
17 modulators, semiconductor optical amplifiers, photodiodes and other photodetectors,  
18 NxN optical switches, and so forth. Examples of passive devices may include but are  
19 not limited to wavelength division multiplexers/de-multiplexers, wavelength division  
20 slicers/interleavers, wavelength division add/drop filters, other optical filters,  
21 splitters/combiners, interferometers, phase shifters, dispersion compensators, fixed or  
22 variable optical attenuators, and so forth. Use of such optical devices involves  
23 transferring optical power or optical signal between the device (within its package) and a  
24 transmission waveguide (part of the optical telecommunications system, often an optical  
25 fiber or other low-loss optical waveguide).

26 **[0011]** Conventional hermetic packaging for such optical devices is typically bulky and  
27 expensive to implement. Devices are typically packaged one-by-one only after  
28 fabrication, assembly, and testing/characterization of the individual devices. The  
29 package itself, including necessary optical and/or electrical feed-throughs, is often far  
30 more voluminous than the device itself (and the sensitive surfaces thereof that

1 necessitate the hermetic package in the first place), the large packaged volume  
2 generally being forced by the nature of the packaging processes. Constraints imposed  
3 by the packaging process and/or materials often require compromises to be made in the  
4 optical design and/or configuration of the device, perhaps satisfying material  
5 compatibility and/or tolerance/stability requirements at the expense of optical device  
6 performance, for example. The packaging process is generally labor intensive, typically  
7 involving separate steps for positioning the device, establishing optical and electrical  
8 connections, and then sealing the package.

## SUMMARY

**[0012]** A method for micro-hermetic packaging of an optical device comprises: a) forming a micro-hermetic cavity on a substrate; b) providing a transmission optical waveguide on the substrate for enabling transfer of optical power between the interior and the exterior of the micro-hermetic cavity; and c) sealing the optical device within the micro-hermetic cavity to form a micro-hermetic package. A lid or substrate separate from the first substrate may be employed for the sealing process, or the micro-hermetic cavity may be provided on the lid and sealed onto the first substrate. An optical device may be positioned within the cavity for optical power transfer with the optical waveguide, and sealed within the micro-hermetic cavity. The device may alternatively be provided on the lid. The micro-hermetic cavity may be fabricated of a size comparable to the optical device, and many such cavities may be simultaneously fabricated on a single substrate using wafer-scale processing. The transmission optical waveguide provides an optical feed-through, and may be provided with the micro-hermetic cavity on the same substrate, or may be provided as a separate component and/or on a separate lid or substrate. Electrical feed-throughs may be provided on the substrate with the micro-hermetic cavity, as a separate component, on a lid, and/or on a separate substrate. Additional functionality for monitoring/controlling the optical device may be provided on the substrate with the micro-hermetic cavity, and/or on a lid or separate substrate.

**[0013]** An embedding or encapsulating medium may be employed for securing optical assemblies and protecting various optical surfaces thereof. Such embedding may serve as a micro-hermetic package and/or may also serve to enhance optical properties/performance of the packaged optical device.

**[0014]** Objects and advantages of micro-hermetic packaging apparatus and methods, as disclosed and/or claimed herein, may become apparent upon referring to the disclosed exemplary embodiments as illustrated in the drawings and disclosed in the following written description and/or claims.

## BRIEF DESCRIPTION OF THE DRAWINGS

**[0015]** Fig. 1A is a top view of an planar waveguide substrate with a ring for micro-hermetic packaging.

**[0016]** Fig. 1B is a top view of an optical device on a device substrate.

**[0017]** Fig. 1C is a top view of the device of Fig. 1B assembled onto the substrate of Fig. 1A.

**[0018]** Fig. 1D is an isometric view of the assembled device of Fig. 1C with a lid for micro-hermetic packaging.

**[0019]** Figs. 2A-2B are top and side views, respectively, of an exemplary optical waveguide and a portion of a micro-hermetic package.

**[0020]** Figs. 3A-3B are top and side views, respectively, of an exemplary optical waveguide and a portion of a micro-hermetic package.

**[0021]** Figs. 4A-4B are top and side views, respectively, of an exemplary optical waveguide and a portion of a micro-hermetic package.

**[0022]** Fig. 5 is a side view of an exemplary optical waveguide and a portion of a micro-hermetic package.

**[0023]** Figs. 6A-6H illustrate exemplary process steps for forming a micro-hermetic package.

**[0024]** Figs. 7A-7K illustrate exemplary process steps for forming a micro-hermetic package.

**[0025]** Figs. 8A-8H illustrate exemplary process steps for forming a micro-hermetic package.

**[0026]** Figs. 9A-9F illustrate exemplary process steps for forming a micro-hermetic package.

**[0027]** Fig. 10 is a top view of an exemplary optical waveguide and micro-hermetic package.

**[0028]** Fig. 11 is a side view of a portion of an exemplary micro-hermetic package.

1 **[0029]** Fig. 12 is a side view of a portion of an exemplary micro-hermetic package.

2 **[0030]** Fig. 13A is a top view of a planar waveguide substrate with a ring for micro-  
3 hermetic sealing.

4 **[0031]** Fig. 13B is a top view of an optical device on a device substrate with a ring for  
5 micro-hermetic sealing.

6 **[0032]** Fig. 13C is a side cross-section view of the device of Fig. 13B assembled onto  
7 the substrate of Fig. 13A.

8 **[0033]** Figs. 14A-14E illustrate exemplary embodiments of an optical waveguide and  
9 micro-hermetic package.

10 **[0034]** Figs. 15A-15C illustrate an exemplary embodiment of an optical waveguide and  
11 micro-hermetic package.

12 **[0035]** The embodiments shown in the Figures are exemplary, and should not be  
13 construed as limiting the scope of the present disclosure and/or appended  
14 claims. It should be noted that the relative sizes and/or proportions of  
15 structures shown in the Figures may in some instances be distorted to facilitate  
16 illustration of the disclosed embodiments.

## 1 DETAILED DESCRIPTION OF EMBODIMENTS

2 **[0036]** Figs. 1A-1D illustrate micro-hermetic packaging of an exemplary optical device.  
3 The exemplary optical device shown may be fabricated and assembled as disclosed in  
4 earlier-cited App. No. 10/187,030, App. No. 60/360,261, and App. No. 60/334,705.  
5 Alternatively, the apparatus and methods disclosed herein may be applied to optical  
6 device assemblies of any suitable configuration. An optical device 110 and integral  
7 external-transfer optical waveguide 130 are provided on device substrate 102, and  
8 substrate 102 is then assembled onto a substantially planar waveguide substrate 122,  
9 substrate 122 having fabricated thereon a planar transmission optical waveguide 120  
10 which may include a core (not shown). Also fabricated on substrate 122 are  
11 contacts/electrodes 160 and alignment/ support structures 170. A proximal end of  
12 waveguide 120 is adapted for transverse-transfer of optical power (adiabatic or mode-  
13 interference-coupled) with the external-transfer optical waveguide 130 on substrate 102,  
14 which is "flip-chip" mounted onto waveguide substrate 122. A distal end of waveguide  
15 120 may be adapted for substantially adiabatic mode-expansion (through tapering of the  
16 core, for example) and end-transfer of optical power to an end of a single-mode optical  
17 fiber (not-shown; may be received in groove 150). Alternatively, waveguide 120 may be  
18 otherwise adapted for optical power transfer to another optical waveguide or device in  
19 any suitable manner (including end-transfer and/or transverse-transfer), and/or may be  
20 one of multiple optical waveguides being provided on substrate 122 and comprising a  
21 portion of a more complex planar waveguide circuit (also referred to as a planar  
22 lightwave circuit, or PLC) on waveguide substrate 122.

23 **[0037]** An electrically insulating packaging or sealing ring 180 is preferably fabricated  
24 onto waveguide substrate 122 along with waveguide 120 and groove 150 (if present).  
25 Ring 180 serves to form a micro-hermetic cavity on substrate 122. Electrical  
26 contacts/electrodes may extend beneath ring 180 to provide electrical feed-throughs to  
27 the device 110 after hermetic sealing. Planar transmission optical waveguide 120 may  
28 pass through ring 180 to form an optical feed-through to device 110 after hermetic  
29 sealing. The upper surface of ring 180 may be provided with a thin metal coating (that  
30 may be wetted by molten solder) and lid 190 may be soldered onto ring 180, thereby  
31 hermetically sealing optical device 110, external-transfer optical waveguide 130, and the

1 proximal portion of planar transmission optical waveguide 120 within the micro-hermetic  
2 cavity formed by waveguide substrate 122, ring 180, and lid 190. If sealed by soldering,  
3 the underside of the lid may preferably be provided with a thin metal coating (that may  
4 be wetted by solder) for soldering on at least the area of the underside corresponding to  
5 the top surface of ring 180, while an interior portion of the lid (corresponding to the  
6 micro-hermetic cavity) may preferably be masked or otherwise prevented from being  
7 wetted by solder. The upper surface of ring 180 should preferably be substantially  
8 planarized to facilitate sealing, although a solder re-flow process may form a seal over  
9 surfaces with small height variations.

10 **[0038]** Lid 190 may be metal, dielectric, ceramics (including multi-layer ceramics),  
11 semiconductor, combinations thereof (including multi-layered materials), and/or  
12 functional equivalents thereof. The underside of lid 190 may be provided with one or  
13 more recessed portions and/or relief cuts for accommodating structures within the  
14 hermetically sealed cavity that might extend as high as or higher than ring 180. Lid 190  
15 may in fact be provided with a sealing ring (not shown), in addition to or instead of a  
16 sealing ring 180 on substrate 122. In the case that sealing rings are provided on both  
17 lid 190 and substrate 122, the rings should preferably mate to form a single micro-  
18 hermetic cavity. In addition to soldering, lid 190 may be sealed onto ring 180 in any  
19 suitable way, including but not limited to: soldering, welding (using a CO2 laser or  
20 otherwise), adhesives, wafer-bonding and/or similar techniques, thermal compression  
21 bonding, solder-glass bonding, combinations thereof, and/or functional equivalents  
22 thereof.

23 **[0039]** Sensitive optical surfaces of optical device 110, external-transfer optical  
24 waveguide 130, and the proximal portion of planar transmission optical waveguide 120  
25 are protected from contamination and/or corrosion due to humidity and/or the presence  
26 of contaminants, which may typically arise through exposure to an uncontrolled use  
27 environment. This is of particular importance for maintaining desired levels of  
28 transverse-transfer of optical power between external-transfer optical waveguide and  
29 planar transmission optical waveguide 120. Such transverse-transfer of optical power  
30 can be sensitive to contamination of the waveguide surfaces involved. Hermetic sealing  
31 may also serve to: protect semiconductor surfaces and/or facets; to protect metal-



1 coated areas such as electrical conductors, electrodes, contacts, feed-throughs, and/or  
2 optical coatings; to inhibit or prevent galvanic corrosion; to inhibit or prevent ionic  
3 migration; to enhance thermal stability of the sealed device. It should be noted that  
4 micro-hermetic packaging methods and apparatus as disclosed herein are not limited to  
5 packaging of devices employing transverse-transfer of optical power, or devices  
6 assembled onto the substrate as shown in Figs. 1A-1D. Any optical devices and/or  
7 waveguides employing optical power transfer by transverse-transfer and/or end-transfer  
8 may be hermetically packaged according to the present disclosure. Any optical devices  
9 and/or waveguides integrated or assembled onto a substrate and connected to an  
10 optical transmission system through one or more planar optical waveguides on the  
11 substrate may be hermetically packaged according to the present disclosure.

12 **[0040]** Ring 180 may be fabricated from any substantially electrically insulating  
13 material capable of providing an adequate barrier against moisture and/or  
14 contaminants. Insulating material is preferred for the exemplary configuration of Figs.  
15 1A-1D so as not to short out contacts/electrodes 160. If electrical feed-throughs are  
16 provided in some other way, non-insulating material(s) may also be used to fabricate  
17 ring 180. Materials and processes used for fabricating ring 180 should preferably be  
18 compatible with the precision material fabrication/processing techniques used to  
19 fabricate planar transmission optical waveguide 120 and other associated structures  
20 that might be present (i.e., contacts/ electrodes 160, alignment/support structures 170,  
21 other optical waveguides, integrated optical devices, and so on) on substrate 122.  
22 These techniques may include but are not limited to: lithography, etching, deposition,  
23 masking, doping, spin coating, and so forth. Employing such techniques not only  
24 enables precision positioning of ring 180 with respect to waveguides 120 and 130,  
25 device 110, and other associated structures, but also enables fabrication and precision  
26 positioning of many (hundreds or thousands) of planar transmission optical waveguides  
27 120 and corresponding rings 180 and other associated structures simultaneously on a  
28 single substrate or wafer, which may be subsequently divided to form finished optical  
29 apparatus. The practical advantages and economies of scale of such wafer-scale  
30 fabrication and/or processing are well known. Suitable materials for ring 180 may  
31 include silica, silica-based materials, polymers including polyimide, ceramics,

1 semiconductors, metals, combinations thereof, and/or functional equivalents thereof  
2 satisfying the above-stated mechanical, chemical, dielectric, and/or fabrication  
3 requirements.

4 **[0041]** The description of the sides of the micro-hermetic package as a "ring" may be  
5 generalized to include a package in which portions of the substrate outside the ring are  
6 at the same height as the ring (see Figs. 14A-14C and 15A-15C). Instead of a micro-  
7 hermetic cavity formed within a protruding ring, the micro-hermetic cavity is formed  
8 within a depression or recess in an otherwise substantially flat substrate. Such an  
9 embodiment may offer advantages and/or economies of fabrication and/or assembly,  
10 particularly since a larger area may be available for sealing a lid over the micro-hermetic  
11 cavity. Throughout the present disclosure, whenever a "ring" is referred to for forming a  
12 micro-hermetic cavity, such a cavity may equivalently be formed instead as a cavity or  
13 recess, or the micro-hermetic cavity may be formed by a combination of a recessed  
14 portion of a substrate surrounded by a protruding ring.

15 **[0042]** An optical device and associated waveguides, contacts, and so forth packaged  
16 according to the present disclosure may be significantly less voluminous than optical  
17 devices packaged by previous techniques, and may typically require substantially fewer  
18 parts. An optical device in a micro-hermetic package according to the present  
19 disclosure may nevertheless be placed within a secondary package that outwardly  
20 resembles previous device packages. Such a secondary package need not be  
21 hermetically sealed and may therefore be provided much more economically than  
22 previous hermetic packages, but would provide mechanical compatibility with existing  
23 optical transmission systems and equipment. In other words, devices packaged  
24 according to the present disclosure (and then enclosed within an appropriate secondary  
25 package) could be readily interchanged with existing devices packaged according to  
26 previous hermetic packaging techniques. However, the significantly reduced packaged  
27 volume of an optical device packaged according to the present disclosure may be  
28 exploited for reducing the overall size of next-generation optical transmission systems  
29 and/or equipment by using the micro-hermetic-packaged devices without secondary  
30 packaging.

1 **[0043]** The intersection of planar transmission optical waveguide 120 and ring 180  
2 warrants further consideration. The presence of ring 180 around waveguide 120 may  
3 disrupt transmission of optical power through waveguide 120 if not properly designed.  
4 One simple means for reducing any such disruption is to provide waveguide 120 with  
5 sufficiently thick cladding around core 124 at the point where waveguide 120 passes  
6 through ring 180. Such thick cladding may also be desirable for the portion of  
7 waveguide 120 that extends outside ring 180 (i.e., outside the hermetic cavity).  
8 However, for transverse-transfer of optical power between waveguide 120 and the  
9 external-transfer waveguide 130, core 124 may typically be fairly close to the surface of  
10 waveguide 120. Figs. 2A-2B, 3A-3B, and 4A-4B illustrate various configurations and  
11 fabrication processes for introducing thicker cladding for waveguide 120 at ring 180 and  
12 outside ring 180, while leaving thinner cladding inside ring 180 for enabling transverse-  
13 transfer. The thicker cladding should preferably be introduced sufficiently gradually that  
14 its appearance does not substantially interfere with transmission of optical power  
15 through waveguide 120 (i.e., adiabatic condition substantially satisfied, as defined in  
16 earlier-cited App. Nos. 10/187,030 and 60/360,261).

17 **[0044]** In Figs. 2A-2B, an upper cladding layer of substantially uniform thickness is  
18 deposited on waveguide 120 (exemplary overall waveguide dimensions are several  $\mu\text{m}$   
19 wide and several  $\mu\text{m}$  thick) and core 124 (exemplary dimensions are several  $\mu\text{m}$  wide  
20 and several tens of nm thick, beneath about  $0.5 \mu\text{m}$  of cladding). Exemplary core and  
21 cladding materials are silicon nitride and germanium-doped silica, respectively, although  
22 many other core/cladding material combinations and/or dimensions may be equivalently  
23 employed (including cores having a lower aspect ratio). The upper cladding layer is  
24 preferably sufficiently thick so that an evanescent portion (extending above the  
25 cladding) of any optical power propagating through the waveguide negligibly affects the  
26 level of optical power transmission through the waveguide (i.e., any decrease in optical  
27 power transmission is within operationally acceptable limits, whatever those may be for  
28 the given circumstances). Spatially-selective masking/ deposition/etching (and/or other  
29 suitable spatially-selective material processing techniques) may be employed to provide  
30 an obliquely beveled lateral surface for this layer, which cuts across waveguide 120 at a  
31 shallow angle within ring 180. The thicker cladding therefore gradually appears along a

1 portion of the length of waveguide 120 without substantially disturbing transmission of  
2 optical power therethrough (substantially adiabatic, within operationally acceptable  
3 limits). The thick upper cladding layer thus deposited may substantially confine  
4 transmitted optical power sufficiently far from the surface of waveguide 120 so that ring  
5 180 and environmental factors outside ring 180 only affect optical power transmission  
6 within operationally acceptable limits. The waveguide 120 and the thick upper cladding  
7 layer may be fabricated in a process separate from fabrication of ring 180, or may occur  
8 concurrently with fabrication of ring 180. In the latter case, ring 180 and the thick upper  
9 cladding layer may in fact form parts of a contiguous structure. The thick upper  
10 cladding should preferably extend no farther vertically than the height of ring 180 (at  
11 least at the point of intersection of waveguide 120 and ring 180), so that lid 190 may  
12 properly form a seal with ring 180.

13 **[0045]** In Figs. 3A-3B, an upper cladding layer of increasing thickness is deposited on  
14 waveguide 120 and core 124 (materials and dimensions similar to the previous  
15 example; other material combinations and/or dimensions may be equivalently  
16 employed). The upper cladding is preferably sufficiently thick (where the waveguide  
17 120 passes through the ring 180) to maintain any resulting decrease in optical power  
18 transmission within operationally acceptable limits. Spatially-selective masking/  
19 deposition/etching (and/or other suitable spatially-selective material processing  
20 techniques) may be employed to provide an upper cladding layer of gradually increasing  
21 thickness (i.e., vertically tapered) with increasing distance from the proximal end of  
22 waveguide 120 within ring 180. The vertically tapered upper cladding layer may be  
23 fabricated in a sequence including multiple deposition steps, may be fabricated using  
24 grayscale lithography techniques; or may be fabricated by any other suitable processing  
25 sequence. The thicker cladding gradually appears along a portion of the length of  
26 waveguide 120 without substantially disturbing transmission of optical power  
27 therethrough (substantially adiabatic, within operationally acceptable limits). The thick  
28 upper cladding layer thus deposited may substantially confine transmitted optical power  
29 sufficiently far from the surface of waveguide 120 so that ring 180 and environmental  
30 factors outside ring 180 only affect optical power transmission within operationally  
31 acceptable limits. The waveguide 120 and the thick upper cladding layer may be

1 fabricated in a process separate from fabrication of ring 180, or may occur concurrently  
2 with fabrication of ring 180. In the latter case, ring 180 and the thick upper cladding  
3 layer may in fact form parts of a contiguous structure. The thick upper cladding should  
4 preferably extend no farther vertically than the height of ring 180 (at least at the point of  
5 intersection of waveguide 120 and ring 180), so that lid 190 may properly form a seal  
6 with ring 180.

7 **[0046]** In Figs. 4A-4B, waveguide 120 is fabricated with two cores 124a and 124b.  
8 Materials and dimensions may be similar to the previous examples; other material  
9 combinations and/or dimensions may be equivalently employed. Core 124a is provided  
10 near the top of waveguide 120 (beneath about 0.5  $\mu\text{m}$  of cladding) at the proximal end  
11 of waveguide 120. Core 124b is provided deeper within waveguide 120 (beneath  
12 several  $\mu\text{m}$  of cladding; same overall waveguide thickness) at the distal end thereof.  
13 Waveguides 124a and 124b are adapted for transverse-transfer of optical power  
14 therebetween (adiabatic or mode-interference-coupled; adiabatic shown in Figs. 4A-4B)  
15 within an intermediate portion of waveguide 120 within ring 180. In this way transmitted  
16 optical power may be substantially confined sufficiently far from the surface of  
17 waveguide 120 so that ring 180 and environmental factors outside ring 180 only affect  
18 optical power transmission within operationally acceptable limits. The waveguide 120  
19 may be fabricated in a process separate from fabrication of ring 180, or may occur  
20 concurrently with fabrication of ring 180. In the latter case, ring 180 and the thick upper  
21 cladding layer may in fact form parts of a contiguous structure.

22 **[0047]** In some instances it may be possible to avoid the structures and procedures  
23 described in the preceding paragraphs. For example, if transverse-transfer of optical  
24 power is not employed by any of the optical components or waveguides within ring 180  
25 and therefore none of the waveguides has a thin-clad portion, then the ring may be  
26 fabricated over waveguide 120 without substantially disturbing transmission through the  
27 waveguide. Alternatively, the walls of ring 180 may be sufficiently thin (compared to the  
28 transverse spatial mode size characteristic of waveguide 120) that transmission of  
29 optical power through waveguide 120 will be sufficiently undisturbed even without a  
30 thicker upper cladding layer. In this instance ring 180 may be fabricated over  
31 waveguide 120, and any optical loss thereby induced simply tolerated (if within

1 operationally acceptable limits). Alternatively, a reflective coating 182 (a thin metal  
2 reflector coating or a multi-layer dielectric reflector coating) may be deposited on the  
3 short segment of waveguide that will be covered by ring 180 (Fig. 5). This may  
4 sufficiently reduce disruption by ring 180 of optical power transmission through  
5 waveguide 120. Such a coating may only be present between ring 180 and waveguide  
6 120, or may appear and disappear substantially adiabatically along the length of  
7 waveguide 120 (see Fig. 6H, for example).

8 **[0048]** The particular waveguide type and material(s) employed for the transmission  
9 waveguide and material(s) employed for the sealing ring may require specifically  
10 tailored fabrication and/or processing sequences. A variety of examples of such  
11 sequences are disclosed herein for particular materials and waveguide types, but  
12 should not be construed as limiting the scope of inventive concepts disclosed and/or  
13 claimed herein. It should be pointed out that in many instances where uniform layer  
14 deposition followed by spatially-selective material removal is employed for providing a  
15 structure, that structure may often be equivalently provided by spatially-selective  
16 deposition.

17 **[0049]** In the exemplary process sequence illustrated in Figs. 6A-6F, a substantially  
18 planar waveguide substrate (Figs. 6A and 6D), including a substrate layer 622a, an  
19 optical buffer layer 622b, and a waveguide material layer 622c, is processed to  
20 spatially-selectively remove at least a portion of the waveguide material layer (and  
21 perhaps also a portion of the buffer layer), leaving ring 680 and waveguide 620 (Figs.  
22 6B and 6E), the waveguide 620 in this example being an air-guided ridge waveguide. In  
23 this example layer 622a may be silicon, layer 622b may be substantially un-doped silica,  
24 and layer 622c may be germanium-doped silica having a higher index than layer 622b.  
25 Any other suitable materials or material combinations may be employed, provided buffer  
26 layer 622b has a lower index than layer 622c. Alternatively, if substrate layer 622a has  
27 a lower index than layer 622c, then buffer layer 622b could potentially be omitted. The  
28 interior portion of waveguide 620 (i.e., the portion within the ring 680) may be adapted in  
29 any suitable manner for interacting with other waveguides, optical components, and/or  
30 optical devices within ring 680. Similarly, the exterior portion of waveguide 620 may be  
31 adapted in any suitable manner for interacting with other waveguides, optical

1 components, and/or optical devices. The upper surface of ring 680 may be provided  
2 with a thin metal coating 682 for allowing soldering of a lid (Figs. 6C and 6F), or may be  
3 otherwise adapted for sealing a lid. As shown in the cross-section of Fig. 6G, the  
4 underside of lid 690 may be provided with a recessed central portion to eliminate  
5 contact with the top surface of waveguide 620. To further reduce the effect of the metal  
6 coating 682 on optical power transmission through waveguide 620, the metal coating  
7 682 may extend along waveguide 620 (in either or both directions from the  
8 waveguide/ring intersection), and may be configured to gradually appear along a portion  
9 of the length of waveguide 620. For example, in Fig. 6H the edge of the metal coating  
10 682 is shown cutting across waveguide 620 at an oblique angle, thereby maintaining a  
11 substantially adiabatic condition along waveguide 620. Other configurations for  
12 introducing metal coating 682 while maintaining substantially adiabatic conditions or  
13 otherwise reducing the impact of the metal coating on optical power transmission may  
14 be implemented while remaining within the scope of inventive concepts disclosed and/or  
15 claimed herein.

16 **[0050]** The exemplary process illustrated in Figs. 7A-7I may be employed for providing  
17 a waveguide comprising a core and lower-index cladding, in which the core does not  
18 substantially disturb the flatness of the upper surface of the waveguide. Starting with  
19 the material layers 722a (substrate), 722b (buffer), and 722c (cladding) analogous to  
20 those of Figs. 6A and 6D, a core 724 may be provided by: spatially-selectively providing  
21 a thin-film core (Fig. 7D) having a thickness of only several tens of nm, using silicon  
22 nitride or silicon oxynitride in this example, or equivalently employing any suitable thin-  
23 film core material; spatially-selectively increasing the refractive index of the waveguide  
24 to form a core (Fig. 7G), by irradiative densification, dopant diffusion or implantation,  
25 photochemical alteration, and/or photophysical alteration. Once the waveguide core  
26 724 has been thus defined, additional cladding material may be added, thereby  
27 increasing the thickness of layer 722c and embedding core 724 therein (Figs. 7E and  
28 7H). The substrate 722 is then processed to spatially-selectively remove a least a  
29 portion of cladding layer 722c (and perhaps also a portion of buffer layer 722b), leaving  
30 ring 780 and waveguide 720 (Fig. 7B, 7F, and 7I). The upper surface of ring 780 may  
31 be provided with a metal coating 782 for allowing soldering of a lid (Fig. 7C), or may be

1 otherwise adapted for sealing a lid. The underside of lid 790 may be provided with a  
2 central recessed portion for eliminating contact with the upper surface of waveguide 720  
3 (Figs. 7J and 7K), although this may not be necessary if the upper cladding layer of  
4 waveguide 720 is sufficiently thick (as discussed hereinabove). The interior portion of  
5 waveguide 720 (i.e., the portion within the ring 780) may be adapted in any suitable  
6 manner for interacting with other waveguides, optical components, and/or optical  
7 devices within ring 780. Similarly, the exterior portion of waveguide 720 may be  
8 adapted in any suitable manner for interacting with other waveguides, optical  
9 components, and/or optical devices. The intersection of waveguide 720 and ring 780  
10 may be configured in any suitable manner, including those shown in Figs. 2A-2B,  
11 3A-3B, and/or 4A-4B.

12 **[0051]** The exemplary process illustrated in Figs. 8A-8F may be employed for providing  
13 a waveguide comprising a core and lower-index cladding, in which the core alters the  
14 shape of the upper surface of the waveguide. Starting with the material layers 822a  
15 (substrate), 822b (buffer), and 822c (cladding) analogous to those of Figs. 6A and 6D,  
16 an additional core layer may be added, the core layer having an index higher than that  
17 of cladding layer 822c. If cladding layer 822c comprises germanium-doped silica, for  
18 example, the core layer might also comprise germanium-doped silica doped at a higher  
19 level than the cladding so that the core level index is larger than the cladding level index  
20 by an appropriate amount. Other substrate, buffer, cladding, and core material may be  
21 equivalently employed. A waveguide core 824 may be provided by spatially-selective  
22 removal of at least a portion of the core layer, in this example leaving not only a  
23 waveguide core portion 824 but a ring core portion 884 (Figs. 8A and 8D). Once the  
24 waveguide core 824 has been provided, additional cladding material may be added,  
25 thereby increasing the thickness of layer 822c and embedding core 824/884 therein  
26 (Figs. 8B and 8E). However, since the deposition of additional cladding material is  
27 typically nearly conformal, the resulting surface will not be flat. The surface of the  
28 cladding material will have a protruding ridge shape corresponding to the shape of the  
29 underlying core, including a waveguide portion 820 and a sealing ring portion 880, and  
30 the upper surface of the ridge should be substantially flat and therefore able to serve as  
31 a sealing surface for a lid. A portion of the cladding material not lying below the ridges



1 820/880 may be spatially-selectively removed, if desired, and a metal coating 882  
2 provided on the top surface of the ring portion of the ridge 880 to allow soldering of a lid,  
3 or may be otherwise adapted for sealing a lid (Figs. 8C, 8F, and 8G). The underside of  
4 lid 890 may be provided with a central recessed portion for eliminating contact with the  
5 upper surface of waveguide 820 (Fig. 8H), although this may not be necessary if the  
6 upper cladding layer of waveguide 820 is sufficiently thick (see discussion hereinabove).  
7 The interior portion of waveguide 820 (i.e., the portion within the ring 880) may be  
8 adapted in any suitable manner for interacting with other waveguides, optical  
9 components, and/or optical devices within ring 880. Similarly, the exterior portion of  
10 waveguide 820 may be adapted in any suitable manner for interacting with other  
11 waveguides, optical components, or optical devices. The intersection of waveguide 820  
12 and ring 880 may be configured in any suitable manner, including those shown in Figs.  
13 2A-2B, 3A-3B, and/or 4A-4B. The core 884 present within ring 880 will typically reduce  
14 transmission of optical power through waveguide 820 only minimally (since its width is  
15 typically similar to the transverse spatial mode size supported by core 824 of waveguide  
16 820), provided waveguide 820 crosses ring 880 at a sufficiently large angle (greater  
17 than about 20°, preferably greater than about 45°, most preferably near 90°).

18 **[0052]** Some materials employed for fabricating a sealing ring may allow fabrication of  
19 a substantially flat-topped ring over underlying structures that are not necessarily flat, as  
20 in the exemplary process illustrated in Figs. 9A-9F. A protruding ridge transmission  
21 waveguide 920 of any suitable type is provided by any suitable means on substrate 922  
22 (Figs. 9A and 9D). The substrate may then be spin-coated with a polymer layer 986  
23 (Figs. 9B and 9E). The nature of spin-coating and the polymer precursors results in a  
24 substantially flat upper surface of polymer layer 986, despite the presence of protruding  
25 structures beneath. Spatially-selective removal of at least a portion of polymer layer  
26 986 leaves a sealing ring 980 with waveguide 920 therethrough (Figs. 9C and 9F). The  
27 polymer ring 980 may be provided with a metal coating 982 for soldering a lid, or may  
28 be otherwise adapted for sealing a lid (Figs. 9C and 9F). As in previous examples, the  
29 interior, exterior, and intersecting portions of waveguide 920 may be adapted in any  
30 suitable manner dictated by the requirements of the particular optical apparatus being  
31 constructed. A ring could be similarly provided using any other material that may be

1 used to form a substantially flat layer over underlying protruding structures, by spin-  
2 coating, spray-coating, re-flow, or other suitable processes. Such materials may include  
3 but are not limited to polyimide, epoxies, CYTOP (Asahi Glass Company; a poly-  
4 fluorinated polymeric material that may be cross-linked), silicone and silicone-based  
5 materials, spin-on glass materials, siloxane polymers, Cyclotene<sup>TM</sup> (B-staged bis-  
6 benzocyclobutene, Dow), Teflon® AF (DuPont), other polymers, sol-gel materials,  
7 doped silica-based materials, solder-glass, other glasses. Alternatively, many materials  
8 may deposited by a variety of techniques to provide a substantially flat upper surface if  
9 deposited in a sufficiently thick layer (substantially thicker than the underlying  
10 structures). A surface thus provided may be sufficiently flat for enabling subsequent  
11 sealing of a micro-hermetic cavity.

12 **[0053]** Instead of constructing a ring around the transmission waveguide and  
13 associated components and/or structures near the proximal end thereof (i.e., the end  
14 that eventually would end up within a sealing ring), it may be desirable to completely  
15 embed the transmission optical waveguide (or the proximal end thereof) and the  
16 associated components and/or structures. For example, in the preceding example  
17 (Figs. 9A-9F), instead of removing the polymer to form a ring, the polymer could have  
18 been simply left intact (or removed only from the distal end of the transmission  
19 waveguide 1020 on substrate 1022, as in Fig. 10). The embedding material 1086  
20 serves to protect surfaces of the waveguide and other components and/or structures  
21 and maintain them in their properly-aligned operating positions. Preferably, the  
22 embedding material comprises transparent material (at the relevant wavelengths)  
23 having an index less than or about equal to the optical components embedded therein.  
24 In addition to providing protection, the presence of embedding material reduces the  
25 index contrast between the packaged optical device and/or optical waveguides and their  
26 surroundings, and may therefore also serve to reduce optical termination issues and/or  
27 improve the adiabatic nature of any embedded optical transmission components. The  
28 optical properties and/or performance of the packaged optical device and/or  
29 waveguides may therefore be enhanced by the presence of the embedding material.  
30 For example, optical transitions may appear to be more adiabatic and therefore less  
31 lossy, or a given level of adiabaticity may be maintained while reducing the lengths of

1 transition regions. Such embedding, or “potting”, of the transmission waveguide and  
2 other waveguides, optical devices, and/or optical components may be employed when  
3 all of the components are integrated together on the substrate, or may be employed  
4 after components are assembled onto the substrate (as in Figs. 1A-1D, minus ring 180  
5 and lid 190). Suitable materials for embedding waveguides and other optical  
6 devices/components may include but are not limited to the materials listed in the  
7 preceding paragraph. Embedding may performed for many devices simultaneously on  
8 a single substrate (wafer-scale), or alternatively may be performed for individual  
9 devices. Embedding may be non-selective (in which an optical device and all  
10 associated components, waveguides, and/or other structures are embedded together),  
11 or embedding may be selective or sectional, thereby requiring dams, grooves, trenches,  
12 or other similar structures for restricting or directing the flow of the embedding material  
13 (as described hereinabove).

14 **[0054]** Methods and apparatus for micro-hermetic packaging of optical devices have  
15 been described herein primarily in terms of providing a sealing ring and a transmission  
16 waveguide as protruding structures on a substrate, the sealing ring forming the sides of  
17 a micro-hermetic cavity. However, other geometries may be equivalently employed for  
18 forming a micro-hermetic cavity while remaining within the scope of inventive concepts  
19 disclosed and/or claimed herein. For example, to form the exemplary embodiment of  
20 Figs. 14A-14E, procedures analogous to those employed in Figs. 7A-7I are employed.  
21 In the embodiment of Figs. 14A-14E, however, material is only removed from the  
22 interior portion of the “ring” 1480, leaving a depression in the cladding layer 1422c.  
23 Transmission waveguide 1420 with core 1424 is a ridge waveguide within the micro-  
24 hermetic cavity, but is a buried waveguide outside the micro-hermetic cavity. A thin  
25 metal coating 1482 may be applied around the perimeter of the “ring” 1480 for enabling  
26 sealing of a lid. To form the embodiments of Figs. 15A-15C, procedures analogous to  
27 those employed in Figs. 8A-8G are employed. In the embodiment of Figs. 15A-15C,  
28 however, cladding material 1522c is removed only from the interior of the “ring” 1580 to  
29 form a deep ridge waveguide 1520 with core 1524 within the micro-hermetic cavity.  
30 Core 1524 forms a shallow ridge waveguide 1520 outside the micro-hermetic cavity.  
31 Metal film 1582 enables sealing of a lid onto the top of ring 1580. In another alternative

1 embodiment (not shown), a sealing ring may be fabricated as a protruding structure on  
2 a substantially flat surface in which the transmission waveguide is substantially  
3 completely embedded as a buried waveguide.

4 **[0055]** Lid 190 may provide additional functionality. For example, instead of providing  
5 electrical feed-throughs 160 as metal films passing below ring 180 on substrate 122, the  
6 metal films may instead be discontinuous at ring 180. Corresponding metal contacts  
7 194 may be provided on lid 190 which protrude downward and establish electrical  
8 contacts with feed-through conductors 160 (Fig. 11). These contacts 194 may extend  
9 through lid 190 and a metallic film 192 on the top surface of (or within) lid 190 may  
10 establish continuity of the electrical feed-throughs when sealed onto ring 180.

11 Alternatively, contacts may be provided on lid 190 for connecting directly to a metal  
12 contact 104 on device substrate 102 without descending back to substrate 122 (Fig. 12).

13 Alternatively, outside electrical connections may be provided solely through lid 190 to  
14 contacts on device substrate 102 and on substrate 122 within ring 180, with no  
15 conductors on substrate 122 beneath or outside ring 180 (in which case the restriction  
16 that ring 180 must be insulating is relaxed, and ring 180 could be formed from solder or  
17 other metallic material). These alternative electrical feed-through configurations may be  
18 particularly desirable in instances of substrate/ring material combinations for which the  
19 presence of metallic conductors on substrate 122 may degrade mechanical adherence  
20 of ring 180 to substrate 122, or where materials or material processing steps for  
21 providing ring 180 are incompatible with the presence of metal coatings 160. Lid 190  
22 may also carry circuitry for generating, modifying, and/or monitoring electronic signal  
23 provided to device 110 through contacts 194. A transparent lid 190 may provide optical  
24 access to device 110 for monitoring and/or for application of optical control signals. Lid  
25 190 may provide thermal monitoring and/or thermal contact for temperature control, or  
26 may serve as a heat sink. Lid 190 may be implemented using optical bench  
27 technologies for providing additional functionality.

28 **[0056]** In other exemplary embodiments of apparatus and methods for micro-hermetic  
29 packaging of optical devices, a device substrate 202 may also serve as a lid for micro-  
30 hermetic sealing of the optical apparatus. Figs. 13A-13C show a waveguide substrate  
31 222 with a transmission waveguide 220 thereon with a sealing ring 280, electrical

1 contacts 260, and alignment/support members 270. An optical device 210 is shown on  
2 device substrate 202 along with waveguide 230. Substrate 202 is preferably adapted to  
3 engage members 270 so as to position waveguide 220 and 230 for transverse-transfer  
4 of optical power therebetween (although any other manner of optical power transfer  
5 between device 210 and waveguide 220 may be equivalently employed, including end-  
6 transfer). Substrate 202 is also adapted for establishing a seal with the top surface of  
7 ring 280, by soldering (ring 280 and/or substrate 202 being provided with metal coatings  
8 for enabling the same; metal coatings not shown) or by any other suitable sealing  
9 means. Substrate 202 preferably mechanically engages members 270 before engaging  
10 ring 280, with any gap remaining between ring 280 and substrate 202 filled by solder  
11 reflow. In this way accurate positioning of device 210 and waveguide 230 relative to  
12 waveguide 220 does not depend on the accuracy or reproducibility of the soldering  
13 process. Substrate 202 may be provided with a sealing ring 203, thereby forming a lid  
14 with a recessed central portion on the underside, in this case partially occupied by the  
15 device 210 and waveguide 230. A sealing ring 203 thus provided on substrate 202 may  
16 either mate with the sealing ring 280, or completely replace sealing ring 280 (if suitably  
17 adapted to accommodate waveguide 220 therethrough). Fabrication of a sealing ring  
18 203 on device substrate 202 may preferably be achieved using fabrication/processing  
19 techniques compatible with those employed to fabricate device 210 and waveguide 230,  
20 thereby enabling precision alignment thereof. Such precision alignment may be  
21 achieved for multiple devices (tens or hundreds or thousands) and corresponding  
22 sealing rings during concurrent fabrication on a common substrate or wafer. A  
23 combination device substrate and lid 202 may be further adapted for providing electrical  
24 feed-throughs as shown in Figs. 11-12 and described hereinabove, or may provide  
25 circuitry and/or other functionality and described hereinabove.

26 **[0057]** For purposes of the foregoing written description and/or the appended claims,  
27 "index" may denote the bulk refractive index of a particular material (also referred to  
28 herein as a "material index") or may denote an "effective index"  $n_{eff}$ , related to the  
29 propagation constant  $\beta$  of a particular optical mode in a particular optical element by  $\beta =$   
30  $2\pi n_{eff}/\lambda$ . The effective index may also be referred to herein as a "modal index". As  
31 referred to herein, the term "low-index" shall denote any materials and/or optical

1 structures having an index less than about 2.5, while "high-index" shall denote any  
2 materials and/or structures having an index greater than about 2.5. Within these  
3 bounds, "low-index" may refer to: silica ( $\text{SiO}_x$ ), germano-silicate, boro-silicate, other  
4 doped silicas, and/or other silica-based materials; silicon nitride ( $\text{Si}_x\text{N}_y$ ) and/or silicon  
5 oxynitrides ( $\text{SiO}_x\text{N}_y$ ); other glasses; other oxides; various polymers; and/or any other  
6 suitable optical materials having indices below about 2.5. "Low-index" may also include  
7 optical fiber, optical waveguides, planar optical waveguides, and/or any other optical  
8 components incorporating such materials and/or exhibiting a modal index below about  
9 2.5. Similarly, "high-index" may refer to materials such as semiconductors, IR materials,  
10 and/or any other suitable optical materials having indices greater than about 2.5, and/or  
11 optical waveguides of any suitable type incorporating such material and/or exhibiting a  
12 modal index greater than about 2.5. The terms "low-index" and "high-index" are to be  
13 distinguished from the terms "lower-index" and "higher-index", also employed herein.  
14 "Low-index" and "high-index" refer to an absolute numerical value of the index (greater  
15 than or less than about 2.5), while "lower-index" and "higher-index" are relative terms  
16 indicating which of two particular materials has the larger index, regardless of the  
17 absolute numerical values of the indices.

18 **[0058]** For purposes of the foregoing written description and/or the appended claims,  
19 the term "optical waveguide" (or equivalently, "waveguide") as employed herein shall  
20 denote a structure adapted for supporting one or more optical modes. Such  
21 waveguides shall typically provide confinement of a supported optical mode in two  
22 transverse dimensions while allowing propagation along a longitudinal dimension. The  
23 transverse and longitudinal dimensions/directions shall be defined locally for a curved  
24 waveguide; the absolute orientations of the transverse and longitudinal dimensions may  
25 therefore vary along the length of a curvilinear waveguide, for example. Examples of  
26 optical waveguides may include, without being limited to, various types of optical fiber  
27 and various types of planar waveguides. The term "planar optical waveguide" (or  
28 equivalently, "planar waveguide") as employed herein shall denote any optical  
29 waveguide that is provided on a substantially planar substrate. The longitudinal  
30 dimension (i.e., the propagation dimension) shall be considered substantially parallel to  
31 the substrate. A transverse dimension substantially parallel to the substrate may be

1 referred to as a lateral or horizontal dimension, while a transverse dimension  
2 substantially perpendicular to the substrate may be referred to as a vertical dimension.  
3 Examples of such waveguides include ridge waveguides, buried waveguides,  
4 semiconductor waveguides, other high-index waveguides ("high-index" being above  
5 about 2.5), silica-based waveguides, polymer waveguides, other low-index waveguides  
6 ("low-index" being below about 2.5), core/clad type waveguides, multi-layer reflector  
7 (MLR) waveguides, metal-clad waveguides, air-guided waveguides, vacuum-guided  
8 waveguides, photonic crystal-based or photonic bandgap-based waveguides,  
9 waveguides incorporating electro-optic (EO) and/or electro-absorptive (EA) materials,  
10 waveguides incorporating non-linear-optical (NLO) materials, and myriad other  
11 examples not explicitly set forth herein which may nevertheless fall within the scope of  
12 the present disclosure and/or appended claims. Many suitable substrate materials may  
13 be employed, including semiconductor, crystalline, silica or silica-based, other glasses,  
14 ceramic, metal, and myriad other examples not explicitly set forth herein which may  
15 nevertheless fall within the scope of the present disclosure and/or appended claims.

16 **[0059]** One exemplary type of planar optical waveguide that may be suitable for use  
17 with optical components disclosed herein is a so-called PLC waveguide (Planar  
18 Lightwave Circuit). Such waveguides typically comprise silica or silica-based  
19 waveguides (often ridge or buried waveguides; other waveguide configuration may also  
20 be employed) supported on a substantially planar silicon substrate (typically with an  
21 interposed silica or silica-based optical buffer layer). Sets of one or more such  
22 waveguides may be referred to as planar waveguide circuits, optical integrated circuits,  
23 or opto-electronic integrated circuits. A PLC substrate with one or more PLC  
24 waveguides may be readily adapted for mounting one or more optical sources, lasers,  
25 modulators, and/or other optical devices adapted for end-transfer of optical power with a  
26 suitably adapted PLC waveguide. A PLC substrate with one or more PLC waveguides  
27 may be readily adapted (according to the teachings of earlier-cited U.S. App. No.  
28 60/334,705, U.S. App. No. 60/360,261, U.S. App. No. 10/187,030, and/or U.S. App. No.  
29 60/466,799) for mounting one or more optical sources, lasers, modulators, and/or other  
30 optical devices adapted for transverse-transfer of optical power with a suitably adapted

1 PLC waveguide (mode-interference-coupled, or substantially adiabatic, transverse-  
2 transfer; also referred to as transverse-coupling).

3 **[0060]** For purposes of the foregoing written description and/or appended claims,  
4 “spatially-selective material processing techniques” shall encompass epitaxy, layer  
5 growth, lithography, photolithography, evaporative deposition, sputtering, vapor  
6 deposition, chemical vapor deposition, beam deposition, beam-assisted deposition, ion  
7 beam deposition, ion-beam-assisted deposition, plasma-assisted deposition, wet  
8 etching, dry etching, ion etching (including reactive ion etching), ion milling, laser  
9 machining, spin deposition, spray-on deposition, electrochemical plating or deposition,  
10 electroless plating, photo-resists, UV curing and/or densification, micro-machining using  
11 precision saws and/or other mechanical cutting/shaping tools, selective metallization  
12 and/or solder deposition, chemical-mechanical polishing for planarizing, any other  
13 suitable spatially-selective material processing techniques, combinations thereof, and/or  
14 functional equivalents thereof. In particular, it should be noted that any step involving  
15 “spatially-selectively providing” a layer or structure may involve either or both of:  
16 spatially-selective deposition and/or growth, or substantially uniform deposition and/or  
17 growth (over a given area) followed by spatially-selective removal. Any spatially-  
18 selective deposition, removal, or other process may be a so-called direct-write process,  
19 or may be a masked process. It should be noted that any “layer” referred to herein may  
20 comprise a substantially homogeneous material layer, or may comprise an  
21 inhomogeneous set of one or more material sub-layers. Spatially-selective material  
22 processing techniques may be implemented on a wafer scale for simultaneous  
23 fabrication/processing of multiple structures on a common substrate wafer.

24 **[0061]** It should be noted that various components, elements, structures, and/or layers  
25 described herein as “secured to”, “connected to”, “deposited on”, “formed on”, or  
26 “positioned on” a substrate may make direct contact with the substrate material, or may  
27 make contact with one or more layer(s) and/or other intermediate structure(s) already  
28 present on the substrate, and may therefore be indirectly “secured to”, etc, the  
29 substrate.



1 **[0062]** The phrase “operationally acceptable” appears herein describing levels of  
2 various performance parameters of optical components and/or optical devices, such as  
3 optical power transfer efficiency (equivalently, optical coupling efficiency), optical loss,  
4 undesirable optical mode coupling, and so on. An operationally acceptable level may  
5 be determined by any relevant set or subset of applicable constraints and/or  
6 requirements arising from the performance, fabrication, device yield, assembly, testing,  
7 availability, cost, supply, demand, and/or other factors surrounding the manufacture,  
8 deployment, and/or use of a particular optical device. Such “operationally acceptable”  
9 levels of such parameters may therefor vary within a given class of devices depending  
10 on such constraints and/or requirements. For example, a lower optical coupling  
11 efficiency may be an acceptable trade-off for achieving lower device fabrication costs in  
12 some instances, while higher optical coupling may be required in other instances in  
13 spite of higher fabrication costs. The “operationally acceptable” coupling efficiency  
14 therefore varies between the instances. In another example, higher optical loss (due to  
15 scattering, absorption, undesirable optical coupling, and so on) may be an acceptable  
16 trade-off for achieving lower device fabrication cost or smaller device size in some  
17 instances, while lower optical loss may be required in other instances in spite of higher  
18 fabrication costs and/or larger device size. The “operationally acceptable” level of  
19 optical loss therefore varies between the instances. Many other examples of such  
20 trade-offs may be imagined. Optical devices and fabrication methods therefor as  
21 disclosed herein, and equivalents thereof, may therefore be implemented within  
22 tolerances of varying precision depending on such “operationally acceptable”  
23 constraints and/or requirements. Phrases such as “substantially adiabatic”,  
24 “substantially spatial-mode-matched”, “substantially modal-index-matched”, “so as to  
25 substantially avoid undesirable optical coupling”, and so on as used herein shall be  
26 construed in light of this notion of “operationally acceptable” performance.

27 **[0063]** While particular examples have been disclosed herein employing specific  
28 materials and/or material combinations and having particular dimensions and  
29 configurations, it should be understood that many materials and/or material  
30 combinations may be employed in any of a variety of dimensions and/or configurations  
31 while remaining within the scope of inventive concepts disclosed and/or claimed herein.

1 **[0064]** It is intended that equivalents of the disclosed exemplary embodiments and  
2 methods shall fall within the scope of the present disclosure and/or appended claims. It  
3 is intended that the disclosed exemplary embodiments and methods, and equivalents  
4 thereof, may be modified while remaining within the scope of the present disclosure  
5 and/or appended claims.